Finite-Time Convergence Stability of Lur'e Discrete-Time Systems

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Abstract: In this paper, a constructive design methodology for Finite-Time Stability (FTS) of a class of nonlinear discrete-time systems is proposed. A dead-beat controller that can achieve *n*-finite-time stability is constructed. Furthermore, stability conditions, based on the use of Borne and Gentina practical stability criterion and matrices in the Benrejeb arrow form, are synthesized. Similarity between transient behaviors of dead-beat controlled linearized and nonlinear third order systems are shown and concluding remarks are formulated.

Keywords: Discrete Lur'e Postnikov systems; Finite-time stability; Dead-beat control; Vector norm; Benrejeb arrow form matrix.

1. Introduction

Finite Time Stability (FTS) was introduced in the control literature in the Sixties in [14, 35]. Since that, FTS has become one of the most fundamental and challenging problems of the nonlinear control. Finite-time stability (or short-time stability) is a much stronger requirement than classical asymptotic stability. It requires that every solution trajectory of the studied system reaches the origin in a finite time, called settling time [9]. Many approaches were proposed in the literature to solve FTS of nonlinear continuous systems. In [9], a solid development for finite-time stability theory of non-Lipschitzian systems is provided and sensitivity of finite-time-stable systems to perturbations is investigated. Some necessary and sufficient conditions for FTS of systems with the uniqueness of solutions in forward time are given in [25]. In [33], finite-time stability and finite-time boundedness sufficient conditions for systems with polynomial vector fields are provided and computational method checking developed conditions introduced.

Moreover, finite-time control and stabilization techniques have developed, in the last decades, an increasing attention in nonlinear control systems theory [17]. Considered first, in the literature of time-optimal control, one of the main advantages of the finite-time control strategy, is its ability to force a control system to reach a specified target in finite time. By consequence, various theoretical control techniques were developed for different classes of nonlinear continuous systems. In this

context, feedback finite-time stabilization controllers of double integrators systems was considered in [8] and [19], perturbed double integrator systems in [32], chain of integrators systems in [27], higher-order controllable systems in [18], systems with parametric and dynamic uncertainties in [20], large-scale interconnected dynamical systems in [26], stochastic systems in [36] and nonlinear systems which can be represented by affine fuzzy system in [23].

Although the method has potential application to practical discrete-time processes, the study of feedback finite-time stabilizing controllers of discrete-time systems is quite underdeveloped and most of the results in the literature are focused on the linear case. Actually, feedback finite-time stabilizing controllers synthesized for linear perturbed systems in [2], for uncertain linear perturbed systems in [38], for linear time-varying systems in [1] and, for linear systems with time-varying delay in [37]. In the last few years, other contributions on finite-time stabilization of nonlinear discretetime systems have been introduced in [23], for systems which can be represented by affine fuzzy system, and in [15], for a class of lowertriangular nonlinear systems.

In this work, the finite-time stabilization problem for the class of discrete-time nonlinear Lur'e Postnikov systems [24] is considered. A procedure showing how to develop a compensator ensuring the system trajectories convergence to zero, in finite sampling time, is introduced. Transient behaviours of the

controlled nonlinear and linearized systems are then discussed.

This paper is organized as follows. In Section 2, the class of the discrete-time Lur'e Postnikov–type systems is introduced and the problem formally stated. In Section 3, the existence conditions of a state feedback deadbeat controller guaranteeing *n*–FTS convergence of the *n*–order linearized discrete-time system, is provided. In Section 4, sufficient stability conditions for Lur'e system are developed via the Borne and Gentina stability criterion and the Benrejeb arrow form matrix, and the case of a third order Lur'e system discussed. Concluding remarks are provided in Section 5.

2. System Description and Problem Statement

Let consider the class of Lur'e discrete-time system (S) of Figure 1, where $r \in \Re$ denotes the reference input, $\varepsilon(kT_s) \in \Re$ the control error at the instant kT_s denoted ε_k , T_s the sampling time and $y \in \Re$ the output of the closed loop system. $f(\varepsilon_k) \colon \Re \to \Re$ represents a memoryless nonlinear valued function, B_0 a zero order holder and D(s) and N(s) polynomials defined by

$$D(s) = a_0 + a_1 s + \dots + a_n s^n \tag{1}$$

$$N(s) = \lambda_0 + \lambda_1 s + \dots + \lambda_{n-1} s^{n-1}$$
 (2)

Where the coefficients a_i and λ_j for $\forall i=0,1,...,n$ and $\forall j=0,1,...,n-1$, are constant parameters such that $a_n \neq 0$ and N(s) characterizing the nonlinear system state feedback compensator.

The introduced nonlinear discrete time system (S) can be described by the following nonlinear recursive scalar equation

$$S: \ \varepsilon_{k+n} + \sum_{i=1}^{n} a_{i}^{*} (\varepsilon_{k+n-1}) \varepsilon_{k+n-1} = r_{k+n} + \sum_{i=1}^{n} b_{i} r_{k+n-1}$$
 (3)

which, for r=0, becomes

$$S: \varepsilon_{k+n} + \sum_{i=1}^{n} a_i^* (\varepsilon_{k+n-1}) \varepsilon_{k+n-1} = 0$$
 (4)

By noting $x_{i,k}$ the i^{th} component of the state vector $x_k \in \mathbb{R}^n$ at instant kT_s and choosing $x_{n,k} = \varepsilon_k$ and $x_{i,k+1}$, $\forall i = 1, ..., p$ and $\forall p = 2, ..., n$ such that

$$\begin{cases} x_{1,k+1} = -a_n^*(\varepsilon_k) x_{n,k} \\ x_{p,k+1} = -a_{n-p+1}^*(\varepsilon_k) x_{n,k} + x_{p-1,k} \end{cases}$$
 (5)

the corresponding state space studied system description, can be written as

$$S: x_{k+1} = A_{RE}(\varepsilon_k) x_k \tag{6}$$

where the instantaneous characteristic matrix $A_{BF}(\varepsilon_k)$ is expressed in the Frobenius form as

$$A_{BF}(\varepsilon_{k}) = \begin{bmatrix} 0 & \cdots & \cdots & 0 & -a_{n}^{*}(\varepsilon_{k}) \\ 1 & \ddots & \vdots & -a_{n-1}^{*}(\varepsilon_{k}) \\ 0 & \ddots & \ddots & \vdots & \vdots \\ \vdots & \ddots & \ddots & 0 & \vdots \\ 0 & \cdots & 0 & 1 & -a_{1}^{*}(\varepsilon_{k}) \end{bmatrix}$$
(7)

The main aims of this paper is, firstly, to find a dead-beat controller ensuring the FTS convergence of the studied system (4) or (6) – (7), with a transient behavior elimination in a finite sampling time, and, secondly, to compare the finite-time stability efficiencies of the controlled studied nonlinear system with those of the corresponding linearized one.

3. Transient Behavior Elimination of Linear Systems

In classical control engineering [3, 34], deadbeat control [13, 16, 29, 31] is considered as an advanced control design technique, developed in the context of finite time stabilization and finite settling time, which aims to perfectly tracking a step reference in a finite number of sampling periods.

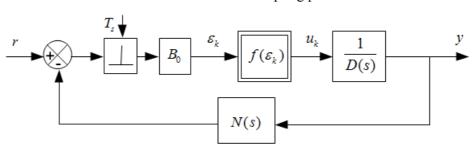


Figure 1. Lur'e discrete-time system

Definition 1. [13] A stabilizing controller of (S) is said to be a dead-beat controller if the tracking error $\varepsilon(kT_s)$ settles down to zero in a finite number of steps $k=N_d$ and $\varepsilon(kT_s)=0$, $\forall k \geq N_d$, where T_s indicates the sampling period and N_d the settling step.

In this section, we provide a methodology to design dead-beat controllers that achieve good transient performance of the linear discrete-time system defined by (3) or by (6) - (7), when the nonlinearity $f(\varepsilon_k)$ is considered constant and equal to K. The main issue to solve this problem, is how to choose the controller parameters λ_i , $i=0,1,\ldots,n-1$ of the polynomial N(s) which guarantee a transient response elimination in n sampling time, where nT_s constitutes the shortest possible settling time of a linear discrete-time control system for a given value of T_s [31].

3.1 Transient elimination in n steps

Let consider the Lur'e system of Figure 1 where the nonlinearity $f(\varepsilon_k)$ is considered constant and equal to K. For r=0, the free system is described by the following equation

$$\varepsilon_{k+n} + \sum_{i=1}^{n} a_i^* \varepsilon_{k+n-1} = 0 \tag{8}$$

such that a_1^* is a linear relation with the controller gains λ_i , $\forall j=0,1,...,n-1$

$$a_i^* = b_i + K \sum_{j=0}^{n-1} a_j^i \lambda_j, \quad \forall i = 1, ..., n$$
 (9)

The nth linear discrete-time system (8) is said to be FTC stable in n sampling time, if the gains λ_j , $\forall j=0,1,...,n-1$ are synthesized, such that ε_{k+n} settles down to zero in n steps, that's equivalent to setting [10, 29, 31]

$$a_i^* \equiv 0 \quad \forall i = 1, 2, \dots, n \tag{10}$$

By solving the system equations (8) it comes the parameters of the state feedback control law characterized by N(s) which guarantees the n-time convergence to zero of the state variables.

3.2 Case of a third order system

3.2.1 System description and analysis

To show the interest of the proposed approach, let consider the third order linear closed loop discrete-time system (S_L) such that f(.) = K and

$$D(s) = s(1 + \tau_1 s)(1 + \tau_2 s) \tag{11}$$

$$N(s)\lambda_0 + \lambda_1 s + \lambda_2 s \tag{12}$$

Where τ_1 , τ_2 , λ_0 , λ_1 and λ_2 are constant parameters. The system is described by

$$S_{L}: \varepsilon_{k+3} + a_{1}^{*} \varepsilon_{k+2} + a_{2}^{*} \varepsilon_{k+1} + a_{3}^{*} \varepsilon_{k} = 0$$
 (13)

Expressions of the coefficients a_3^* , a_2^* and a_1^* are given, respectively by (14), (15) and (16) for f = K.

$$a_{3}^{*} = (\tau_{2} - \tau_{1})^{-1} \times e^{\frac{-T_{s}(\tau_{1} - \tau_{2})}{\tau_{1}\tau_{2}}} \times \left(\tau_{1} - \tau_{2} - f \lambda_{0} (\tau_{1}^{2} - \tau_{2}^{2} - \tau_{1}^{2} d_{1}^{-1} + \tau_{2}^{2} d_{2}^{-1}) + \right) \times \left(\tau_{1} - \tau_{2} - \tau_{1} d_{1}^{-1} + \tau_{2} d_{2}^{-1} + \tau_{2} d_{2}^{-1}\right) + f \lambda_{2} (d_{1}^{-1} - d_{2}^{-1}) - T_{s} f \lambda_{0} (\tau_{1} - \tau_{2})\right)$$
(14)

$$a_{2}^{*} = f \times \left((d_{1}^{-1} d_{2}^{-1})(\tau_{2} - \tau_{1}) \right)^{-1}$$

$$\lambda_{0} \tau_{1}^{2} (1 - d_{1}^{-1} + d_{2}^{-1} - d_{1}^{-1} d_{2}^{-1})$$

$$-2\lambda_{2} d_{1}^{-1} - \lambda_{0} \tau_{2}^{2} \begin{pmatrix} 1 + d_{1}^{-1} - d_{2}^{-1} \\ -d_{1}^{-1} d_{2}^{-1} \end{pmatrix}$$

$$\times +2\lambda_{2} d_{2}^{-1} + \tau_{1} \begin{pmatrix} \lambda_{1} \begin{pmatrix} d_{1}^{-1} - d_{2}^{-1} \\ +d_{1}^{-1} d_{2}^{-1} - 1 \end{pmatrix} \\ +T_{s} \lambda_{0} (d_{1}^{-1} + d_{2}^{-1}) \\ -d_{1}^{-1} - d_{2}^{-1} - 1 \end{pmatrix}$$

$$+\tau_{2} \begin{pmatrix} \lambda_{1} (d_{1}^{-1} - d_{2}^{-1} - d_{1}^{-1} d_{2}^{-1} + 1) \\ -T_{s} \lambda_{0} (d_{1}^{-1} + d_{2}^{-1}) \\ +d_{1}^{-1} + d_{2}^{-1} + 1 \end{pmatrix}$$

$$(15)$$

$$a_{1}^{*} = \left(d_{1}^{-1} d_{2}^{-1} (\tau_{2} - \tau_{1})\right)^{-1} \times \left(d_{1}^{-1} d_{2}^{-1} (\tau_{2} - \tau_{1})\right)^{-1} \times \left(d_{2}^{-1} (d_{1}^{-1} - d_{2}^{-1}) \tau_{1}^{2} + d_{1}^{-1} (1 - d_{2}^{-1}) \tau_{2}^{2}\right) + \left(d_{1}^{-1} + d_{1}^{-1} d_{2}^{-1} + d_{1}^{-1} d_{2}^{-1} + d_{1}^{-1} d_{2}^{-1} + d_{1}^{-1} d_{2}^{-1} + d_{1}^{-1} d_{2}^{-1}\right) - \left(d_{2}^{-1} + d_{1}^{-1} + d_{1}^{-1} d_{2}^{-1} + d_{1}^{-1} d_{1}^{-1} d_{2}^{-1} + d_{1}^{-1} d_{1}^{-1} d_{2}^{-1}\right) + \left(d_{2}^{-1} + d_{1}^{-1} d_{1}^{-1} d_{2}^{-1}\right) + \left(d_{2}^{-1} + d_{1}^{-1} d_{2}^{-1}\right) + \left(d_{2}^{-1} - d_{2}^{-1}\right)$$

$$(16)$$

with
$$d_1^{-1} = e^{\frac{T_s}{\tau_1}}$$
 and $d_2^{-1} = e^{\frac{T_s}{\tau_2}}$

A state space description (S_L) associated to the linear system (8) with (14) – (16) and

developed in the Fobenius canonial form, can be introduced as

$$S_{L}: \begin{bmatrix} z_{k+1} \\ w_{k+1} \\ \varepsilon_{k+1} \end{bmatrix} = \begin{bmatrix} 0 & 0 & -a_{3}^{*} \\ 1 & 0 & -a_{2}^{*} \\ 0 & 1 & -a_{1}^{*} \end{bmatrix} \begin{bmatrix} z_{k} \\ w_{k} \\ \varepsilon_{k} \end{bmatrix}$$
(17)

By applying (10), setting $a_i^*=0$, $\forall i=1,2,3$ and choosing $\lambda_0=1$, the transient behaviour of the closed loop system (13) with (14) – (16) or (17) is eliminated in three sampling periods for K, λ_1 and λ_2 defined, respectively, by

$$K = \left(T_s(1 - d_1)(1 - d_2)\right)^{-1} \tag{18}$$

$$\lambda_1 = \tau_1 + \tau_2 - T_s \frac{(d_1 + d_2 - d_1 d_2)^2 - d_1 d_2}{(1 - d_1)(1 - d_2)}$$
 (19)

$$\lambda_2 = \tau_1 \tau_2 - T_s \frac{\tau_1 d_2^3 (1 - d_1)^2 - \tau_2 d_1^3 (1 - d_2)^2}{(d_1 - d_2)(1 - d_1)(1 - d_2)}$$
 (20)

with
$$d_1 = e^{\frac{T_s}{\tau_1}}$$
 and $d_2 = e^{\frac{T_s}{\tau_2}}$.

Equations (18) – (20) characterize solutions to the FTS problem for the third order nonlinear plant (S_L).

3.2.2 Simulation results

The plant (S_L) is used for simulations where the constant times system are chosen to be τ_1 =0,1 s and τ_2 =0,05 s, the sampling period T_s =0,2 s and the initial conditions $x_1(0)$ =0,1, $x_2(0)$ =0,011 and $x_3(0)$ =-0,073. Satisfaction of the FTS conditions (18) – (20) is accomplished by making the static gain K and the dead-beat controller gains λ_1 and λ_2 , respectively equal to

$$K = K_{FTCS} = 5,89$$
 (21)

$$\lambda_1 = 0.14 \tag{22}$$

$$\lambda_2 = 0.48 \times 10^{-2}$$
 (23)

The system with the given controller parameters is asymptotically stable for the sector domain D_1 , defined by

$$D_1 = \{ K \mid 0.2 \times 10^{-3} < K < 10.35 \}$$
 (24)

as shown in Figsures 2, 3 and 4. With the same control law (12) with (22) – (23), the system dynamics, for $K=K_{FTCS}$, are presented in Figure 2 and, for K=4, in Figure 4. Simulations results for $K=K_{FTCS}$ highlight the three-sampling-time stability convergence (0,6s) of (S_L) , as depicted in Figure 2. By

varying K in D_1 , the system transient behaviour becomes more important than for the particular case $K=K_{FTCS}$. Comparing results of Figure 2 with those of Figure 4, one can note that the stability convergence is obtained for a number of sampling times m, m > 3.

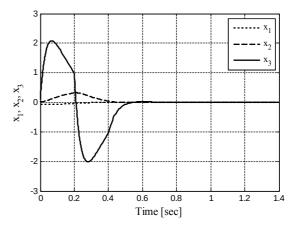


Figure 2. System dynamics for: $K = K_{FTCS}$

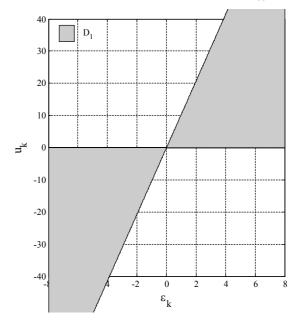


Figure 3. Linear system stability domain

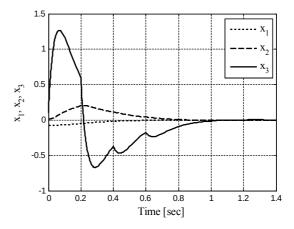


Figure 4. System dynamics for K = 4

4. Stability Convergence Conditions for Nonlinear Systems

Most of stability results of nonlinear Lur'e Postnikov systems focused on frequency analysis: absolute stability [24], Popov criterion [28] and circle criterion [21]. In this section, stability conditions for the Lur'e Postnikov systems (6) - (7) are developed using the Borne and Gentina stability criterion [10-12] (Appendix) and the Benrejeb arrow form matrix [4-7]. Moreover, a stabilizing dead-beat controller for the nonlinear studied system (4) or (6) - (7) exploiting the controller parameters of the linearized system (13) with (14) - (16) or (17) is proposed.

4.1 Lur'e system stability analysis

Let (S) be a Lur'e-type system of the form (4) or (6)-(7), a_j , $\forall j=1,2,...,n-1$, $a_i\neq a_j$, $\forall i\neq j$ be distinct arbitrary constant parameters and β_j , γ_j and γ_n be parameters expressed respectively by [4-7].

$$\beta_{j} = \prod_{\substack{k=1\\k \neq j}}^{n-1} (\alpha_{j} - \alpha_{k})^{-1}, \forall j = 1, ..., n-1$$
 (25)

$$\gamma_{i}(.) = -P_{A_{ne}}(., \alpha_{i}), \forall j = 1,...,n-1$$
 (26)

$$\gamma_n(.) = -a_1(.) - \sum_{i=1}^{n-1} \alpha_i$$
 (27)

 $P_{A_{\rm BF}}(.,\lambda)$ is the instantaneous characteristic polynomial such that

$$P_{A_{BF}}(.,\lambda) = \lambda^{n} + \sum_{i=1}^{n} a_{i}(.) \lambda^{n-1}$$
 (28)

By applying the Borne and Gentina practical stability criterion [11, 12] to the discrete Lur'e type system (4) or (6) - (7) characterized by the Benrejeb arrow form matrix [4-7], it comes the following theorem [30].

Theorem. The Lur'e Postnikov discrete-time system (S) (4) or (6) -(7) is asymptotically stable, if there exists constant parameters α_i , $\forall i, j = 1, 2, ..., n - 1$, $\alpha_i \neq \alpha_j, \forall i \neq j$ and $\varepsilon > 0$ such that $\forall x_k \in D \subset \Re^n$, the following conditions are satisfied

$$|\alpha_i| < 1, \forall i=1,\dots,n-1$$
 (29)

$$1 - |\gamma_n(.)| - \sum_{i=1}^{n-1} |\gamma_j(.)| |\beta_j| (1 - |\alpha_j|)^{-1} \ge \varepsilon$$
 (30)

If $D = \Re^n$, the stability is global.

Proof. Let consider the Lur'e type system (S) of the state representation form (6). A change of coordinate defined by $y_k = Tx_k$ with $y_k \in \mathbb{R}^n$ and $T \in \mathbb{R}^{n \times n}$ inversible, defined by

$$T = \begin{bmatrix} 0 & 0 & \cdots & 0 & 1\\ 1 & \alpha_1 & \cdots & \alpha_1^{n-2} & \alpha_1^{n-1}\\ \vdots & \vdots & \cdots & \vdots & \vdots\\ 1 & \alpha_{n-1} & \cdots & \alpha_{n-1}^{n-2} & \alpha_{n-1}^{n-1} \end{bmatrix}$$
(31)

leads to the following state space description

$$y_{k+1} = A_F(.) y_k$$
 (32)

where $A_F(.)$ is an arrow form matrix given by

$$A_{F}(.) = \begin{bmatrix} \gamma_{n}(.) & \beta_{1} & \cdots & \beta_{n-1} \\ \gamma_{1}(.) & \alpha_{1} & & \\ \vdots & & \ddots & \\ \gamma_{n-1}(.) & & & \alpha_{n-1} \end{bmatrix}$$
(33)

and β_i , γ_j , γ_n and α_i , $\forall i=1,2,\cdots,n-1$ defined respectively in relations (25) – (27) with (28). A pseudo-overvaluing matrix $M(A_F(.))$ of (32), corresponding to the use of the vector norm $p(y_k) = [|y_{1,k}|, |y_{2,k}|, \cdots, |y_{n,k}|]^T$ with $y_k = [y_{1,k}, y_{2,k}, \cdots, y_{n,k}]^T$, for the stability study, such that [12]

$$p(y_{k+1}) \le M(A_F(.))p(y_k) \tag{34}$$

leads to the following comparison system

$$\mathbf{z}_{k+1} = M(A_F(.))\mathbf{z}_k \tag{35}$$

$$M(A_{F}) = \begin{bmatrix} |\gamma_{n}(.)| & |\beta_{1}| & \cdots & |\beta_{n-1}| \\ |\gamma_{1}(.)| & |\alpha_{1}| & & \\ \vdots & & \ddots & \\ |\gamma_{n-1}(.)| & & & |\alpha_{n-1}| \end{bmatrix}$$
(36)

with $M(A_F(.)) \in \mathbb{R}^{n \times n}$, $z_k \in \mathbb{R}^n$ and $z_0 = p(y_0)$. Since the nonlinearities of the comparison nonlinear system (35) are isolated in one row of $M(A_F(.))$, stability conditions are, then, deduced by applying Borne and Gentina stability criterion

$$\begin{pmatrix}
I_n - M(A_F(.)) = \begin{pmatrix}
1 & 2 & \cdots & h \\
1 & 2 & \cdots & h
\end{pmatrix} > 0
\forall h = 1, 2, \dots, n$$
(37)

This completes the proof.

Corollary. If there exists constant parameters $\varepsilon > 0$ and $\alpha_i \in \Re, 0 < \alpha_i < 1, \alpha_i \neq \alpha_k, \forall j \neq k$,

 $j,k=1,\cdots,n-1$ such that $\delta_n(.)>0$ and $\gamma_j(.)\beta_j>0, \forall j=1,\dots,n-1$, then, the nonlinear discrete time system (S) (4) or (6) – (7) is asymptotically stable if the following condition is satisfied

$$P_s(.,\lambda)\big|_{\lambda=1} \ge \varepsilon$$
 (38)

Proof. If there exists constant parameters $\alpha_j \in \mathbb{R}$, $0 < \alpha_j < 1$, $\alpha_j \neq \alpha_k$, $\forall j \neq k$, and $j, k = 1, \dots, n-1$ such that $\delta_n(.) > 0$ and $\gamma_j(.)\beta_j > 0$, $\forall j = 1, \dots, n-1$, then, the comparison system (35) – (36) is identical to the system itself. Linear Aizerman conjecture is, consequently, satisfied. In this case, by substituting (25) – (27), stability condition (30) of (S) becomes

$$\begin{pmatrix}
1+a_1(.)+\sum_{p=1}^{n-1}\alpha_p+\\
+\sum_{p=1}^{n-1}\frac{1}{1-\alpha_p}\left(\frac{(\lambda-\alpha_p)P_s(..\lambda)}{Q(\lambda)}\right)_{\lambda=\alpha_p}
\end{pmatrix}>0$$
(39)

where $Q(\lambda)$ is defined by

$$Q(\lambda) = \prod_{p=1}^{n-1} (\lambda - \alpha_p)$$
 (40)

Now, observing that,

$$\frac{P_{S}(.,\lambda)}{Q(\lambda)} = \lambda + a_{1}(.) + \sum_{p=1}^{n-1} \alpha_{p} + \sum_{p=1}^{n-1} \frac{1}{\lambda - \alpha_{p}} \left(\frac{(\lambda - \alpha_{p})P_{S}(.,\lambda)}{Q(\lambda)} \right)_{\lambda = \alpha_{p}}$$
(41)

stability condition (39) is, then, equivalent to

$$\frac{P_S(.,\lambda)}{Q(\lambda)}\bigg|_{\lambda=1} > 0 \tag{42}$$

or equivalently to

$$P_{S}(.,\lambda)\big|_{\lambda=1}>0 \tag{43}$$

That ends the corollary proof.

4.2 Finite time stability: Case of a third order Lur'e system

We reconsider the nonlinear Lur'e third order system presented in the previous section and introduced in Figure 1 with (11) and (12). The system can be described by the following recursive equation

$$S: \varepsilon_{k+3} + a_1^*(\varepsilon_{k+2})\varepsilon_{k+2} + a_2^*(\varepsilon_{k+1})\varepsilon_{k+1} + a_3^*(\varepsilon_k)\varepsilon_k = 0$$

$$(44)$$

where the expressions of the parameters $a_3^*(.)$, $a_2^*(.)$ and $a_3^*(.)$ depending on the nonlinearity f are defined respectively by (14), (15) and (16). By using (5), it comes the state space representation

$$S: \begin{bmatrix} z_{k+1} \\ w_{k+1} \\ \varepsilon_{k+1} \end{bmatrix} = \begin{bmatrix} 0 & 0 & -a_3^*(\varepsilon_k) \\ 1 & 0 & -a_2^*(\varepsilon_k) \\ 0 & 1 & -a_1^*(\varepsilon_k) \end{bmatrix} \begin{bmatrix} z_k \\ w_k \\ \varepsilon_k \end{bmatrix}$$
(45)

The dead-beat control for the linearized model (S_L) (13) will, in reality, be applied to the nonlinear model (S) (44), which includes property modifications. The effects of this choice on the FTS property of the resulting feedback system are to be investigated. This investigation will be simplified by representing the nonlinearity around $u_k = K_{FTCS} \varepsilon_k$.

For the defined system constants time and the synthesized controller parameters $(\lambda_0, \lambda_1, \lambda_2)$, the state matrix $A_{BF}(.)$ of (45), expressed in the Frobenius form, is such that

$$A_{BF}(.) = \begin{bmatrix} 0 & 0 & 0.24 \times 10^{-2} - 0.50 \times 10^{-3} f(\varepsilon_k) \\ 1 & 0 & -0.15 + 0.26 \times 10^{-1} f(\varepsilon_k) \\ 0 & 1 & 1.15 - 0.19 f(\varepsilon_k) \end{bmatrix} (46)$$

Now, using the transformation (31) – (35) to (45) with α_1 =0,14 and α_2 =0,02 satisfying (29), the new state matrix of (44) or (45) – (46) is in the Benrejeb arrow form as following

$$A_{F}(.) = \begin{bmatrix} 0.99 - 0.19 f(\varepsilon_{k}) \\ 0.50 \times 10^{-3} - 0.60 \times 10^{-3} f(\varepsilon_{k}) \\ -0.20 \times 10^{-3} - 0.30 \times 10^{-4} f(\varepsilon_{k}) \\ 8.33 - 8.33 \\ 0.14 & 0 \\ 0 & 0.02 \end{bmatrix}$$
(47)

Stability condition of (S) characterized by (44) or (45) - (46), deduced from the developed Theorem, is then

$$\begin{vmatrix} 1 - \left| 0.99 - 0.19 f(\varepsilon_k) \right| - \\ -9.68 \times 10^{-3} \times \left| 0.50 - 0.6 f(\varepsilon_k) \right| - \\ -8.5 \times 10^{-3} \times \left| -0.02 - 0.03 \times 10^{-1} f(\varepsilon_k) \right| \end{vmatrix} > 0$$

equivalent to

$$D_2:0.30\times10^{-3} < f(.) < 9.88$$
 (48)

For purposes of comparison with the linearized system (S_L) behaviour, let consider the nonlinear function $f(\varepsilon_k) = c_1 \left(\varepsilon_k + c_2 \sin(\varepsilon_k)^p\right)$

and study the influence of the constant parameters c_1 , c_2 and p, on the elimination time of the transient. Three cases are introduced in Table 1.

Table 1. Parameters definition of $f(\varepsilon_k)$

	c_1	c_2	p
Case 1	4	0.5	2
Case 2	5.89	0.5	2
Case 3	5.89	0.7	5

The responses of the system, with the cases 1, 2 and 3 of $f(\varepsilon_{\nu})$, are shown for initial values of $x(0)=[0.1, 0.011, -0.073]^T$ in, respectively, Figures 5, 7 and 9. As shown in cited Figures, $f(\varepsilon_k)$ is in the sector characterized by (48) for all considered cases. The corresponding system controller stabilizes the Lur'e system (S) as illustrated in Figures 6, 8 and 10. For case 1, (S) remains stable but looses the proper of three sampling period convergence to zero, as shown in Figure 6. For cases 2 and 3, the nonlinear functions vary around the line $u_k = K_{FTCS} \varepsilon_k$ and the transient behaviour is eliminated in three sampling periods, as shown in Figures 8 and 10. Figure 11 compares the response of the linearized and nonlinear (case 2) systems. When u_k is around $K_{FTCS} \varepsilon_k$, the (S_L) and (S)responses are nearly identical. Else, the responses are significantly different, the system is FTS in n+m step times with m>0.

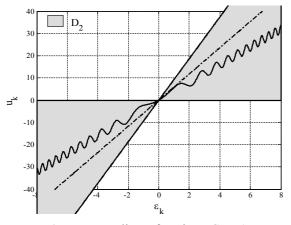


Figure 5. Nonlinear function - Case 1

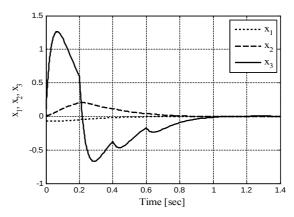


Figure 6. System dynamics - Case 1

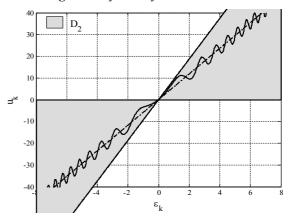


Figure 7. Nonlinear function- Case 2

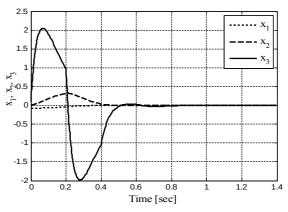


Figure 8. System dynamics - Case 2

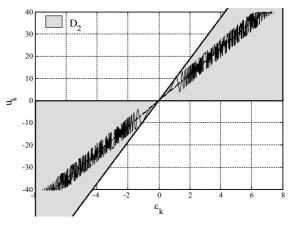


Figure 9. Nonlinear function - Case 3

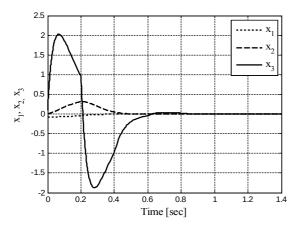


Figure 10. System dynamics - Case 3

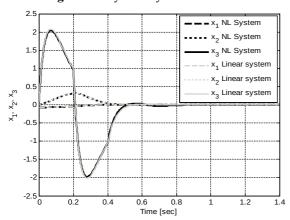


Figure 11. Linearized and nonlinear (Case2) System dynamics

5. Conclusion

The design approach considered in this paper, is based on specifying an *n*–FTS behavior for the Lur'e type nonlinear systems via the linearized system dead-beat controller. Although, this does not guarantee an *n*–FTS behavior in general case, linearization approaches have proved successful in many practical situations in literature. Validity of the proposed method was illustrated with success via an example of a third order Lur'e system.

Appendix

Definition 2. (Vector Norm) Let $E=\Re^n$ be a vector space and E_1, E_2, \dots, E_k subspaces of E which verify: $e=E_1\cup E_2\cup \dots \cup E_k$. Let $x\in E$ be an n vector defined on E with a projection in the subspace E_i denoted by x_i , $x_i=P_ix$, where P_i is a projection operator from E into E_i . Let p_i be a scalar norm $(i=1,\dots,k)$ defined on the subspace E_i $p_i(x):\Re^n \to \Re^k_+$ and p(x)

denotes the vector norm of dimension k with $p(x) = \begin{bmatrix} p_1^T(x) & p_2^T(x) & \dots & p_k^T(x) \end{bmatrix}^T$.

Kotelyanski Lemma [22]. The real parts of the eigenvalues of matrix A, with non negative off diagonal elements, are less than a real number μ if and only if all those of matrix $M = \mu I_n - A$ are positive, with I_n the n identity matrix. When successive principal minors of matrix (-A) are positive, Kotelyanski lemma permits to conclude on stability property of the system characterized by A.

Borne and Gentina practical stability criterion [11, 12]. Let consider the nonlinear discrete system

$$\mathbf{z}_{k+1} = A(.)\mathbf{z}_k \tag{49}$$

and the overvaluing matrix $M(A(.)) \in \mathbb{R}^{n \times n}$ associated to the use of the vector norm p_z defined by $p_z = [|z_{1,k}|, |z_{2,k}|, \dots, |z_{n,k}|]^T$ with $z_k = [z_{1,k}, z_{2,k}, \dots, z_{n,k}]^T$ and such that

$$M(A(.))=\{|a_{j,k}|\}, \quad \forall j, k=1,\dots,n$$
 (50)

If the nonlinearities are isolated in either one row or one column of M(A(.)), the verification of the Kotelyanski condition enables to conclude to the stability of the original system characterized by A(.).

The system (49) is asymptotically stable if all successive principal minors of $(I_n-M(A(.)))$ are positive.

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